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Mass of MgO that could be added as backfill in theWIPP and the mass of MgO required to saturate the brine and react with the CO₂ generated by microbial processes.

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1) Brym Reviewer:

<u>3/11/96</u> Date

Reviewer: <u><u><u></u></u> Yifeng Wang</u>

<u>3/5/96</u> Date

SWCFA:WBS 1.1.01.2: Source Term:Backfill Calculations

Scope of Analysis

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The objectives of this analysis is to calculate the mass of MgO backfill that could be emplaced in the total free volume of the WIPP, calculate the amount of MgO required to react will all the CO_2 generated from microbial processes, and calculate the amount of MgO that will be dissolved in Castile brine and a mixture of 90% Castile and 10% Salado Brine.

This analysis was performed by hand calculations using information from the literature.

Andrew C. Peterson performed these calculations.

The following assumptions are made.

The bulk density of MgO is 0.5 of the crystalline density.

The volume of brine to be chemically controlled is 1.0×10^6 m³.

(This assumption is based on personal communication from Kurt Larson)

The brine composition is (a) 100% Castile or (b) 90% Castile and 10% Solado.

The RH waste was not considered because of emplacement in walls of the disposal rooms above the room floor.

1.) Mass of MgO Backfill

The volume will be determined from the total volume less the air space above the waste and the volume of the waste.

Total volume of a room is equal to the width times the length times the height (less the 0.711 meters of air space). (Appendix A is pg. 3-13 from WIPP PA, 1991).

Width = 10.06 m Length = 91.44 m Height = 3.251 m

Room Volume = $(10.06)*(91.44)*(3.251) = 2,990.55 \text{ m}^3$

Appendix A shows the dimensions of a 7-Pack. The length of each side of this regular 6 sided polygon is equal to

 $l = (1.65/2)/Cosine 30^\circ = 0.825/0.866 = 0.953 m$

The area of a regular 6 sided polygon is equal to Area = $(1/4)*6*l^2*Cot(180^{\circ}/6) = 0.25*6*0.953^2*1.7321 = 2.36 \text{ m}^2$

From Appendix A, the height of a 7 Pack is the height of the drum plus the height of two slip sheets. height = 0.892 + 2 (0.004) = 0.900 m

7- Pack Volume = $(2.36)*(0.900) = 2.124 \text{ m}^3$

From Appendix A the drum external diameter is 0.602 m and the height is 0.892 m. The external volume is equal to :

Volume = $(3.1416)*(0.602)^{2}*(0.892)/4 = 0.2539 \text{ m}^{3}$

Free Volume per 7- Pack = (7-Pack Volume)-Volume of 7 Drums - volume of slip sheets. = $(2.124 - 7*(0.2539)-2*0.004*2.36 = 0.3278 \text{ m}^3$

Number of 7-Packs per room = No. per length * No per Width * No per height = 54*6*3=972 (Appendix A)

Free Volume per Room = Total volume-Total 7 Pack volume + Free volume per 7-Pack =2,990.55-(972)*(2.124)+(972)*(0.3278) = 1,245 m³

The number of rooms is about 120. (WIPP PA, 1991, pg. 3-5)

The Total Free Volume in the WIPP = $120 * 1,245 = 149,400 \text{ m}^3$

Mass of MgO that could be emplaced in the Free Volume

The density of crystalline MgO is 3.58 gm/cm³ (Lide, 1995)

Assume the bulk density of MgO is 50% of the crystalline density.

Bulk Density = $(0.5)*(3.58g/cm^3)*(10^6 cm^3/m^3) = 1.79 * 10^6 gm/m^3$

Mass of MgO emplaced = Free Volume * Bulk Density = $149,040 \text{ m}^3 * 1.79*10^6 \text{ gm/m}^3 = 2.67*10^{11} \text{ gms}$

The molecular wight of MgO is 40.3.

Total Moles of MgO emplaced = $2.67*10^{11}$ gm/(40.3 gm/mole) = $6.62*10^{9}$ moles

2.) Moles of MgO dissolved in brines

Castile

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The concentration in Castile brine was estimated from an EQ3NR calculation by Yifeng Wang. Appendix B contains the first page of the input file and the calculated concentration of Mg^{++} .

As shown in Appendix B, the maximum concentration of Mg^{++} was about 0.02 moles per kg of H₂O.

As is also shown in the input file in Appendix B, the initial Mg⁺⁺ concentration was 0.019 moles per kg of H_2O

The initial concentration of total dissolved salts, as shown in Appendix B, was $3.33*10^5$ mg of salts/liter of brine (0.333 kg/l) and the density was 1.216 gms/cm³ (1.216 kg/l).

The mass of salts per kg of brine = (0.333 kg of salt/l)/1.216 kg of brine/l = 0.27 kg of salt/kg of brine.

Mass of H₂ O per kg of brine = Total - mass of salt = 1.0 - 0.29 = 0.73 kg H₂O/ kg brine

The volume of the brine to be chemically controlled is 10^6 m^3 .

The moles of MgO dissolved in Castile brine

=change in concentration*density H_2O/kg brine*brine volume = (0.020-0.019)mole/kg H₂O*1.216 kg brine/1*0.73 kg H₂O/kg brine*10*⁶ m³ *10³l/m³ = 8.88*10⁵ moles

Salado

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The concentration in Salado brine was also estimated from an EQ3NR calculation by Yifeng Wang. Appendix C contains the first page of the input file and the calculated concentration of Mg^{++} . As shown in Appendix C, the concentration was about 1 mole/kg of H₂O after the addition of MgO.

The initial concentration, as show in Appendix C, was 1.44 mole/kg of H₂O.

The addition of MgO resulted in a decrease in the final concentration Mg⁺⁺.

A mixture of 90% Castile brine and 10% Salado brine would dissolve 90% of the amount for Castile brine

The amount dissolve would equal

 $=0.90*(8.88*10^5 \text{ moles})=7.99*10^5 \text{ moles}$

3.) Estimate of moles of CO₂ generated by microbial activity

Inventory Report (DOE, 1995) will be used to estimate the amount of cellulosics, rubbers, and plastics in the inventory. The method of Wang and Brush (1996) will be used to convert to weights of plastics and rubbers into moles of C produced.

DOE, 1995 reports the following weights for an average drum of CH TRU waste

Cellulosics = 54 kg/m^3 Rubber = 10 kg/mPlastics = 34 kg/m^3 Container Plastic = 26 kg/m^3

Based on the method of Wang and Brush 1996 the total estimated weight of equivalent celluolosics is Cellulosis = 54 kg/m^3

Rubber = 10 kg/m^3

Plastic = $1.7*(34 \text{ kg/m}^3) = 57.8 \text{ kg/m}^3$ Plastic/liner = $1.7*(26 \text{ kg/m}^3) = 44.2 \text{ kg/m}^3$ Total Cellulosics = $54 + 10 + 57.8 + 44.2 = 166 \text{ kg/m}^3$

The total volume of CH waste (DOE 1996, pg. 3-3) is 1.6*10⁵ m³

The total cellulosics in the WIPP = $(166 \text{ kg/m}^3)^*(1.6^*10^5 \text{ m}^3) = 2.656^*10^7 \text{ kg}$

A molecular weight of 162 was used by Wang and Brush (1996) for all cellulosics.

The total moles of C, based on the method of Wang and Brush (1996), pg. 15

= (weight of equivalent cellulosics /molecular weight of cellulosics)*number of C per mole

 $= ((2.656*10^7 \text{ kg})*(1000 \text{ gm/kg})/(162 \text{ gms/mole}))*(6) = 9.84 * 10^8 \text{ moles of C}.$

The maximum amount of CO₂ generated would be one mole for each mole of C in the waste.

Total MgO required for dissolving in brine and reacting with CO₂ generated by microbial activity.

Castile Brine

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Dissolved = 8.88×10^5 moles.

The maximum CO_2 generated from microbial activity = 9.84×10^8 moles

One mole of MgO is required for each mole of CO₂ generated.

Total MgO required = $8.88 \times 10^5 + 9.84 \times 10^8 = 9.85 \times 10^8$ moles

Volume of MgO = $(9.85*10^8 \text{ moles}*40.3 \text{ gms/mole})/1.79*10^6 \text{ gms/m}^3 = 22,176 \text{ m}^3$

Wang and Brush 1996a estimated that 0.04% of the cellulose would be converted by denitrification, 0.01% converted by sulfate reduction, and 95% converted by methanogenesis. Denitrification and sulfate reduction generate on mole of CO_2 for each mole of cellulose and methanogenesis generates one half mole of CO_2 for each mole of cellulose. Based on this estimate the total amount of CO_2 generated would equal

Moles of $CO_2 = (0.04 + 0.01 + 0.95/2)*9.84*10^8 = 5.17*10^8$ moles.

Total MgO required = $8.88 \times 10^5 + 5.17 \times 10^8 = 5.18 \times 10^8$ moles

Volume of MgO = $(5.18 \times 10^8 \text{ moles} \times 40.3 \text{ gms/mole})/1.79 \times 10^6 \text{ gms/m}^3 = 11,662 \text{ m}^3$

Total MgO available if all of the 149,400 m^3 of free volume was fill with MgO was previously calculated to be $6.62*10^9$ moles.

Mixture of 90% Castile brine and 10% Salado Brine

Dissolved = 7.99×10^5 moles

Maximum CO₂ generated = $9.84*10^8$ moles

Total MgO required = $7.99 \times 10^5 + 9.84 \times 10^8$ moles = 9.85×10^8 moles

Volume of MgO = $(9.85*10^8 \text{ moles}*40.3 \text{ gms/mole})/1.79*10^6 \text{ gms/m}^3 = 22,176 \text{ m}^3$.

Using the estimates of Wang and Brush for the expected microbial processes which resulted in $5.17*10^8$ moles of CO₂ being generated the

Total MgO required = $7.99 \times 10^5 + 5.17 \times 10^8 = 5.18 \times 10^8$ moles.

Volume of MgO = $(5.18 \times 10^8 \text{ moles} \times 40.3 \text{ gms/mole})/1.79 \times 10^6 \text{ m}^3 = 11,662 \text{ m}^3$

References

Department of Energy (DOE), 1995. Transuranic Waste Baseline Inventory Report (Revision 2). DOE/CAO-95-1121. Carlsbad New Mexico.

Lide D. R. (1995) Handbook of Chemistry and Physics. CRC.

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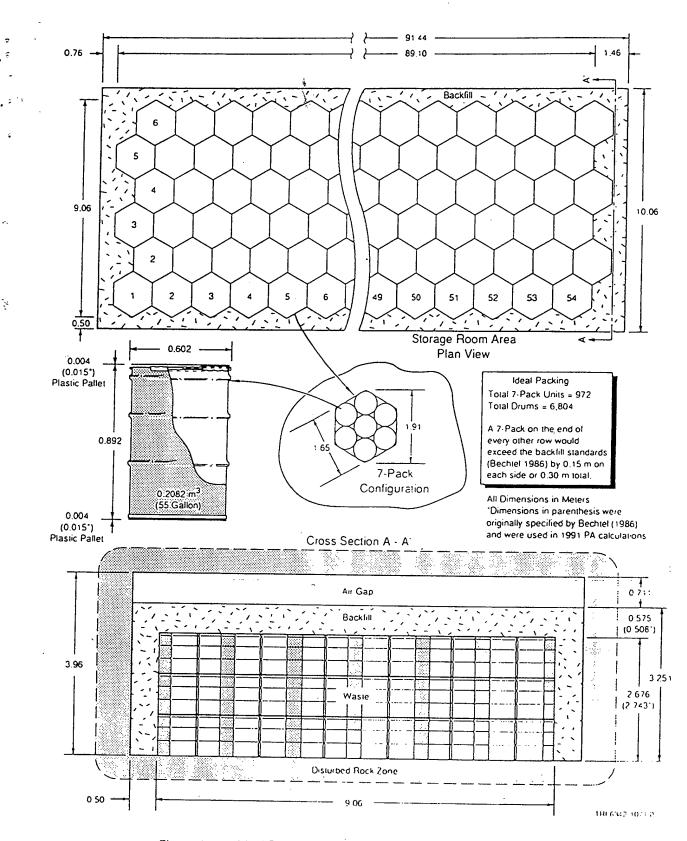
WIPP PA (Performance Assessment) Division 1991. Preliminary Comparison with 40 CFR Part 191, Subpart B for the Waste Isolation Pilot Plant, December 1991. Volume 3: Reference Data. SAND91-0893/3. Albuquerque, NM Sandia National Laboratories.

Wang, Yifeng and Larry Brush, (1996). Estimates of Gas-Generation Parameters for the Long-Term WIPP Performance Assessment, Sandia National Laboratories, Albuquerque, NM. (Memo to Martin Tierney, January 26, 1996).

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Appendix A

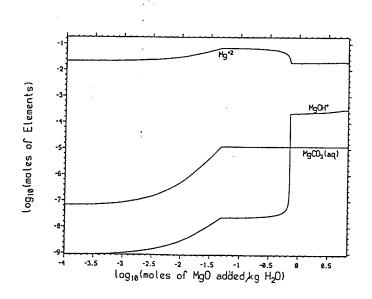
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Figure 3.1-3. Ideal Packing of Drums in Rooms and 10 m wide Drifts.

	Арр	endix B					
EQ3NR input file name= Description= "erda6" Control Version level= 7.2 Created 1/26/96 Cre	erda6.3i				-		
Purpose: to calculate for a given pH. The ad are calculated from t	total dissolve ctivity coeffic	ed inorganic cient of the	aqueous s	species			
Temperature (C)	25.00	Density(g	m/cm3) 1	1.21600	-		
Total Dissolved Salts	3.33E+05	mg/kg *	mg/l no	ot used	-		
Electrical Balancing on	Electrical Balancing on code selects *not						
SPECIES	BASIS SWITCH	I/CONSTRAINT	CONC/ETC	C UNITS (OR TYPE		
redox Na+ K+ Ca++ Mg++ H+ HCO3- Cl- SO4 Input Solid Solutions			70000 4.8700 0.09700 0.01200 0.0190 6.1700 0.0160 4.8000 0.17000	LogfO2 Molarity Molarity Molarity pH Molarity Molarity Molarity	7 7 7		
none							
SUPPRESSED SPECIES (su	ppress,replace	,augmentk,au	igmentg)	value			
			suppress		0.		
Dolomite mineral suppress OPTIONS - SOLID SOLUTIONS - * ignore solid solutions process hypothetical solid solutions - LOADING OF SPECIES INTO MEMORY - * does nothing lists species loaded into memory - ECHO DATABASE INFORMATION - * does nothing lists all reactions lists reactions and log K values lists reactions, log K values and polynomial coef. - LIST OF AQUEOUS SPECIES (ordering) - * in order of decreasing concentration in same order as input file - LIST OF AQUEOUS SPECIES (concentration limit) - * all species only species > 10**-20 molal only species > 10**-12 molal not printed - LIST OF AQUEOUS SPECIES (rement) FION ONLY B.1							



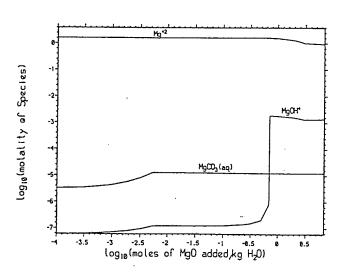
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	EQ3NR input file name= B Description= "Brine A"	RN A.3i								
، • •	Version level= 7.2 Created 1/26/96 Creator= Yifeng Wang									
ie s	Purpose: to calculate total dissolved inorganic carbon in the brine for a given pH. The activity coefficient of the aqueous species are calculated from the HMW equation and related equations.									
• * ''	Temperature (C)	25.00	Density(g	m/cm3)	1.20000					
÷	Total Dissolved Salts	3.06E+05	mg/kg *	mg/1	not used					
	Electrical Balancing on			code s	elects *not pe	erformed				
<u></u>	SPECIES	BASIS SWITCH/	CONSTRAINT	CONC/E	TC UNITS OF	R TYPE				
Pet	redox Na+ K+ Ca++ Mg++ H+ HCO3- Cl- SO4			70000 1.8300 0.77000 0.02000 1.4400 6.5000 0.0100 5.3500 0.04000	Molarity Molarity Molarity Molarity pH Molarity Molarity					
	Input Solid Solutions none SUPPRESSED SPECIES (sup	press, replace,	augmentk,au	l 1gmentg)	 value					
	Dolomite	mineral		suppres	 5S	0				
	OPTIONS									
	 SOLID SOLUTIONS - ignore solid solution process hypothetical process input and hyp LOADING OF SPECIES INTO does nothing lists species loaded ECHO DATABASE INFORMATINATION (Construction) (Co	solid solution pothetical solid D MEMORY - into memory ION - og K values K values and p (ordering) - ig concentration (concentration (concentration 0 molal 2 molal	oolynomial on on limit) -	coef.	J					
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